

# Multi-Modal Flow in a Thermocoupled Model of the Antarctic Ice Sheet, with Verification

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(note: *MINOR ADDITIONS TO TALK AS GIVEN*)

# Outline

- 1 Continuum model for multi-modal thermocoupled flow
- 2 Verification
- 3 Inputs to the model (for Antarctica)
- 4 Some preliminary results for current state of Antarctica

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# Goldsby-Kohlstedt (2001) constitutive relation

Used in the interior of the ice sheet

## Four flow regimes

Each term is like Arrhenius-Glen-Nye flow law, but with different stress exponent. Note  $\dot{\epsilon}$  is 2nd invariant of strain rate tensor  $\dot{\epsilon}_{ij}$ .

$\dot{\epsilon}_{\text{diff}}$	diffusion creep ( $n = 1$ )	grain size dependent
$\dot{\epsilon}_{\text{gbs}}$	grain-boundary sliding ( $n = 1.8$ )	grain size dependent
$\dot{\epsilon}_{\text{basal}}$	basal glide ( $n = 2.4$ )	
$\dot{\epsilon}_{\text{disl}}$	dislocation climb ( $n = 4$ )	

## A nontrivial combination

$$\dot{\epsilon} = \dot{\epsilon}_{\text{diff}} + \left( \frac{1}{\dot{\epsilon}_{\text{gbs}}} + \frac{1}{\dot{\epsilon}_{\text{basal}}} \right)^{-1} + \dot{\epsilon}_{\text{disl}}$$

# Glen's flow law

- ① used for ice stream/shelf flow
- ② used for verification
  - time dependent exact solutions to thermocoupled SIA
  - time independent exact solutions for ice streams

## Arrhenius-Glen-Nye form

$$\dot{\epsilon}_{ij} = A(T^*)\sigma^{n-1}\sigma_{ij}$$

$A(T^*)$  softness factor

$T^*$  homologous temperature

$n$  stress exponent

$\sigma_{ij}$  stress deviator tensor

$\sigma$  second invariant of  $\sigma_{ij}$

*we use Paterson and Budd (1982) form for  $A(T^*)$*

# Inverse Glen's flow law needed for shelf/stream flow

## Stress in terms of strain rate

$$\sigma_{ij} = 2\nu(\dot{\epsilon}, T^*)\dot{\epsilon}_{ij}$$

## Effective viscosity

For Glen's flow law,

$$\nu(\dot{\epsilon}, T^*) = \frac{1}{2}A(T^*)^{-1/n}\dot{\epsilon}^{\frac{n-1}{n}}$$

## Note

It is difficult to invert the Goldsby-Kohlstedt flow law.

# Mass-balance and conserv. of energy *solved everywhere*

## Map-plane mass-balance equation

$$\frac{\partial H}{\partial t} = M - \nabla \cdot \mathbf{Q} \quad \text{where } \mathbf{Q} = \bar{\mathbf{U}} H$$

$H$  thickness

$M$  ice-equiv. accum. rate

$\mathbf{Q}$  map-plane hor. flux

$\bar{\mathbf{U}}$  vert.-averaged hor. vel.

## Conservation of energy (temperature) equation

$$\frac{\partial T}{\partial t} + \mathbf{U} \cdot \nabla T + w \frac{\partial T}{\partial z} = K \frac{\partial^2 T}{\partial z^2} + (\text{strain-heating})$$

$T$  ice temperature

$K$  conductivity of ice

$\mathbf{U}$  horizontal velocity

$w$  vertical velocity

# Velocity determined locally for inland (SIA) ice sheet

Get velocity in SIA by vertically-integrating this:

$$\frac{\partial \mathbf{U}}{\partial z} = -2F(\sigma, T^*, \dots) P \nabla h$$

$\sigma = \rho g(h - z)|\nabla h|$  shear stress  $T^*$  homol. temperature

$P = \rho g(h - z)$  pressure  $h$  surface elevation

(Note: Add basal velocity  $\mathbf{U}_b$ , too!)

Note: all isotropic flow laws have form

$$\dot{\epsilon}_{ij} = F(\sigma, T^*, \dots) \sigma_{ij}$$

where “...” might include grain size, pressure, etc.



# Velocity determined “globally” in streams and shelves

## MacAyeal-Morland equations for Glen law

Velocity in ice shelves and streams is depth-independent. Solve a boundary-value problem at each time:

$$[2\nu H(2u_x + v_y)]_x + [\nu H(u_y + v_x)]_y - \beta u = \rho g H h_x$$

$$[2\nu H(2v_y + u_x)]_y + [\nu H(u_y + v_x)]_x - \beta v = \rho g H h_y$$

where effective viscosity *depends on velocity and temperature*:

$$\nu = \frac{\bar{B}}{2} \left[ \frac{1}{2}u_x^2 + \frac{1}{2}v_y^2 + \frac{1}{2}(u_x + v_y)^2 + \frac{1}{4}(u_y + v_x)^2 \right]^{\frac{1-n}{2n}},$$

$$\bar{B} = \left( \text{vertical average of } A(T^*)^{-1/n} \right)$$

# Notes on basal motion: linear (for now)

## Thermally-activated

If the bed temp is below pressure-melting then no sliding.

## Inland ice sheet flow

Assume till has viscosity  $\nu$  and thickness  $L$ . Basal velocity from basal effective shear stress:

$$(\text{basal velocity}) = \frac{L}{\nu} (\text{basal stress})$$

## Ice stream flow

Basal stress determined by friction parameter  $\beta$  ( $\beta = 0$  for shelves):

$$(\text{basal stress}) = \beta (\text{basal velocity})$$

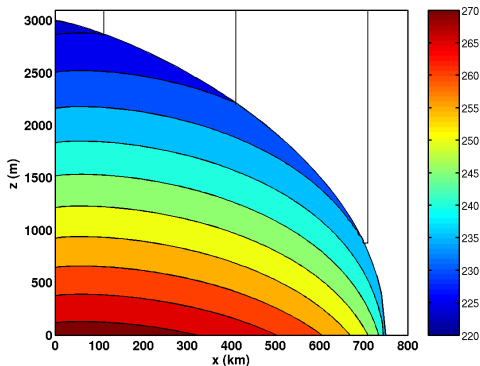
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# Verification of the SIA numerics

## Time-dependent exact solution to thermocoupled SIA equations

$H, T$  chosen  $\longrightarrow$  [compute accumulation, velocity,  
strain-heating, etc.  
which satisfy all eqns]



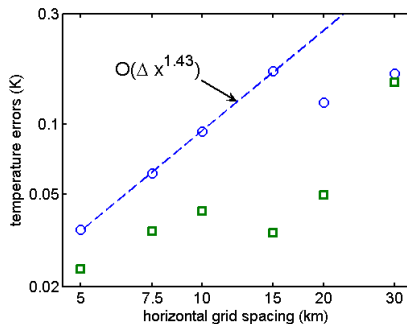
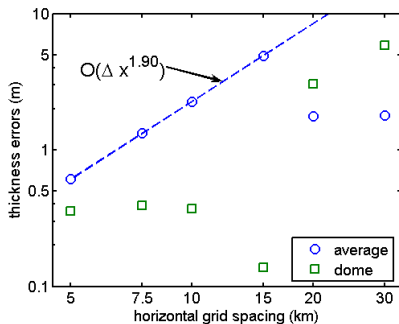
### Reference

Bueler, Kallen-Brown,  
Lingle, *Exact solutions  
to thermocoupled  
ice-sheet models . . .*,  
submitted soon!

# Convergence under grid refinement

Because we know exact solution,

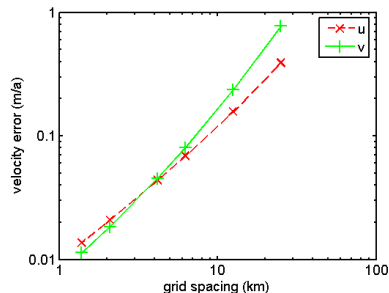
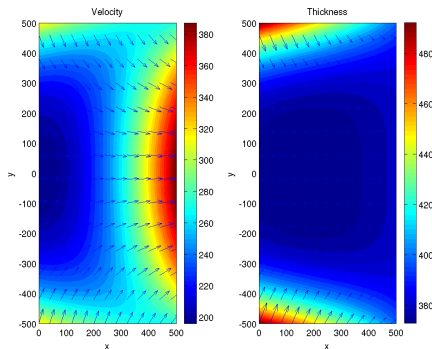
- numerical errors (thickness and temperature) are known and
- convergence rate under grid refinement can be measured.



# Verification of the (dragging) ice shelf numerics

Exact solution to the MacAyeal-Morland equations

$u, v, H$  chosen  $\longrightarrow$  (compute drag which satisfies eqns)



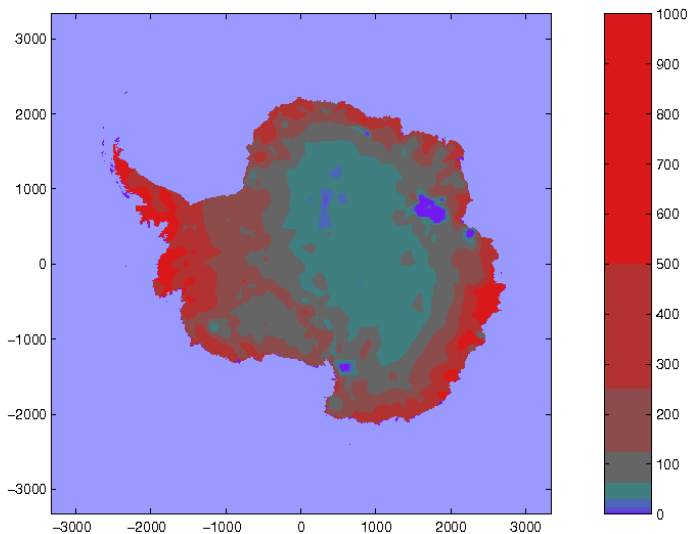
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Inputs to the model

# Accumulation (m/a)

Vaughan et al., 1999, provided by British Antarctic Survey

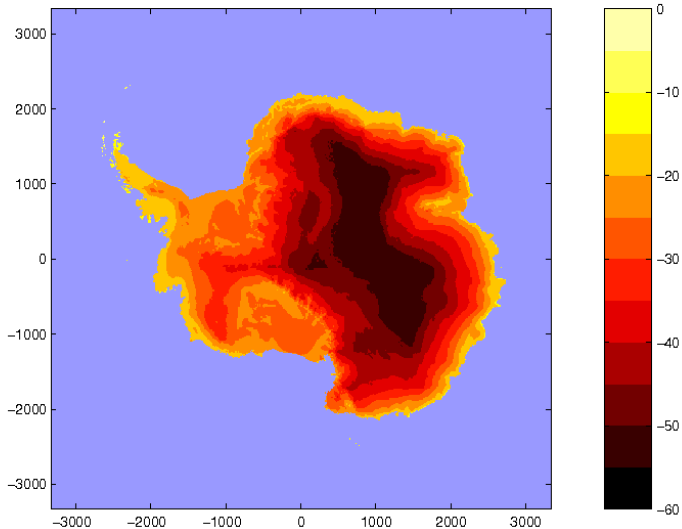




Inputs to the model

# Surface temperature (K)

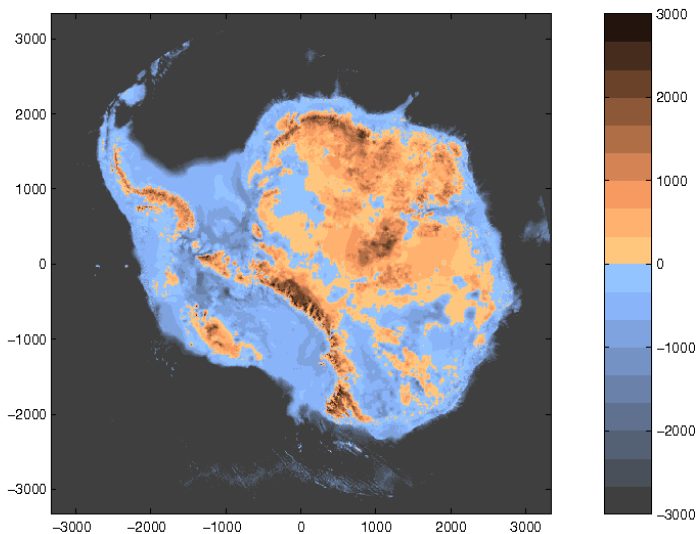
Comiso et al (2000), provided by BAS



Inputs to the model

# Bed elevation (m)

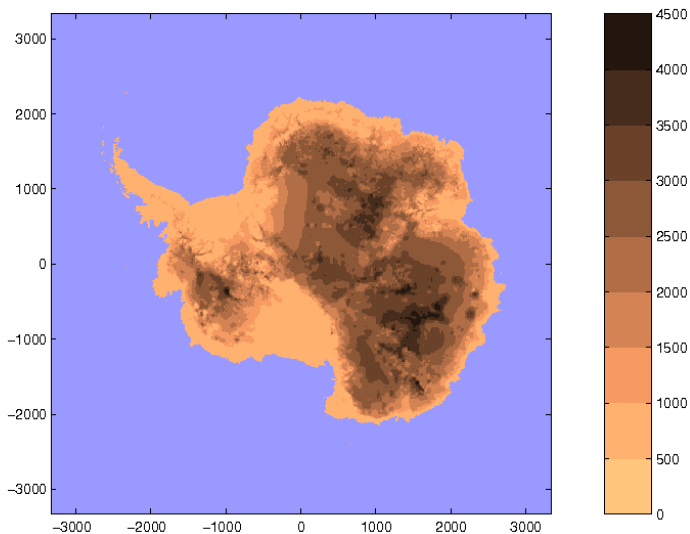
BEDMAP, Lythe et al (2001), provided by BAS



Inputs to the model

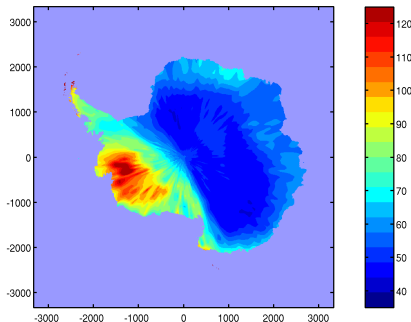
# Thickness (m)

Based on BEDMAP and surface elevations from Liu et al (1999), and provided by BAS

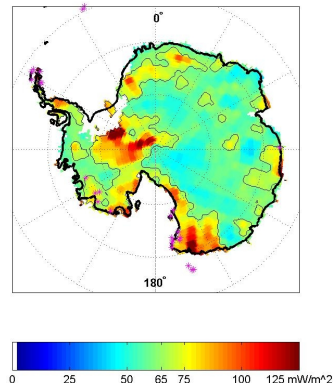


# Geothermal flux ( $\text{mW}/\text{m}^2$ )

Shapiro & Ritzwoller (2004; Earth Planetary Sci. Let.); **results computed from this one:**



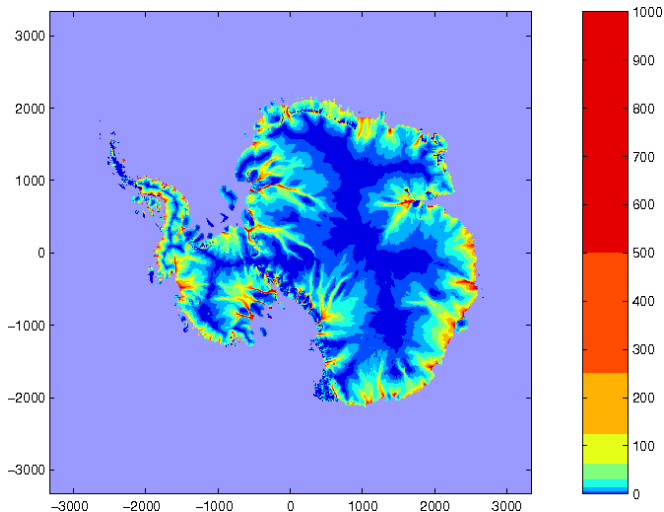
Fox Maule et al. (2005; Science):



Inputs to the model

# Balance velocity is used for flow mode “mask”

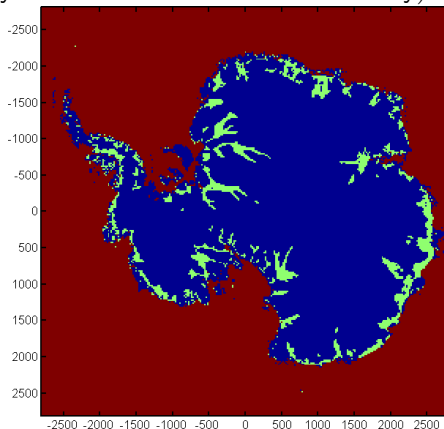
Bamber et al (2000) based on Budd and Warner (1996) algorithm



# The which-type-of-flow mask

Flow type is determined for current state by (sliding velocity) = (balance velocity) – (Goldsby-Kohlstedt deformational velocity):

- **red** if ice is floating (or ice-free ocean)
- **blue** (inland SIA) if (sliding)  $\leq 40 \text{ m a}^{-1}$
- **green** (ice stream) if (sliding)  $> 40 \text{ m a}^{-1}$



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# Initializing a numerical ice sheet model for real ice sheets *means solving obligatory inverse problems*

## Boundary data available to modellers:

surface elevation, thickness, bed elevation, accumulation, surface temperature, geothermal flux [*from other models*], mass-balance velocities [*assumptions plus computations*], ...

## *SPARSE* data at depth (e.g. ice core data)

temperature, age, grain size, basal condition [*very sparse*], ...



# Initializing *means solving inverse problems* cont.

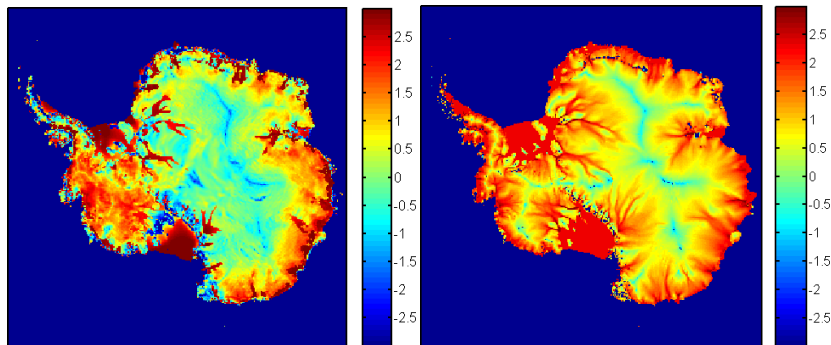
Must “fill in” (or guess) to initialize simulation

- **temperature** (long “spin-up” to meet advection time scale)
- **basal condition** (drag)
- **age and grain size** (needed by G.-K. flow law)

*Reminder:* With above fields, flow equations determine **velocity field**, but velocity field effects temperature and basal conditions. . .

# Modeled horizontal velocity [*preliminary*]

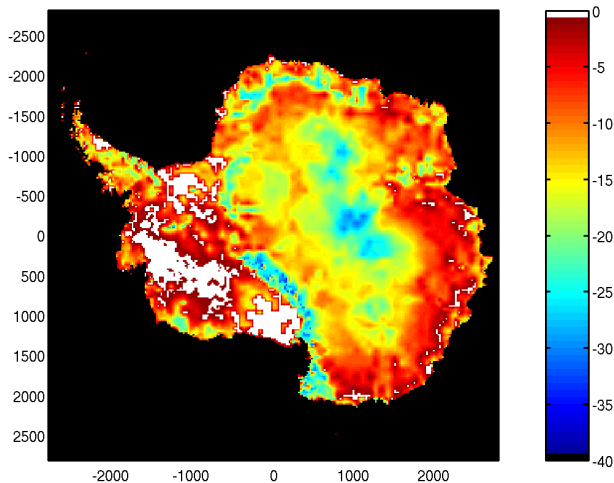
- **left:**  $\log_{10}$  of vertically-averaged horizontal speed
- **right:**  $\log_{10}$  of mass-balance speed (Bamber et al 2000)



Velocity and temperature fields

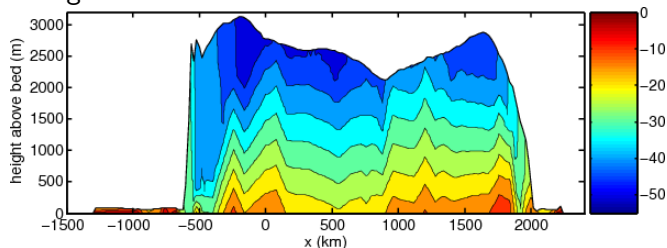
# Modeled basal homologous temperature [*preliminary*]

(degrees C below pressure melting)

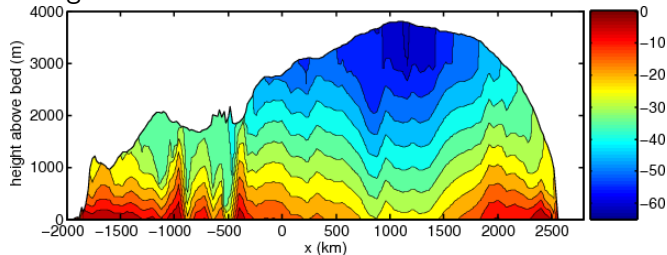


# Modeled temp along sections through S pole [*preliminary*]

Along  $0^{\circ}$ – $180^{\circ}$ :



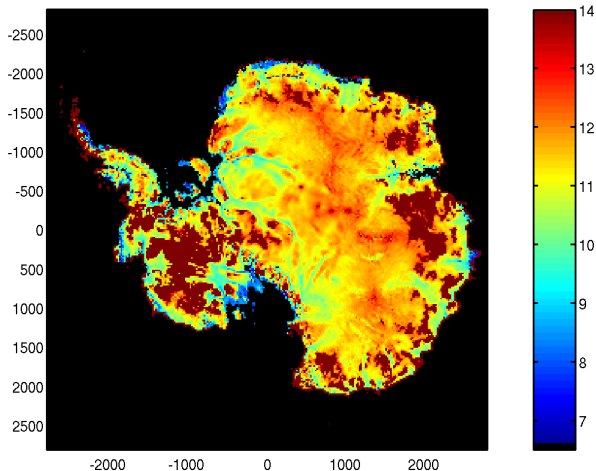
Along  $90^{\circ}$ W– $90^{\circ}$ E:



## Estimation of basal drag

Basal drag assuming linear law:  $(\text{stress}) = -\beta \mathbf{U}_{\text{sliding}}$

$\log_{10}(\beta)$  where  $\beta$  is in units  $\text{Pa s m}^{-1}$ . Compare constant value  $2.0 \times 10^9 \text{ Pa s m}^{-1}$  in (Hulbe and MacAyeal 1998). *Preliminary.*



# How the last slide was created

## Getting basal drag from balance velocities and the SIA

- ① deformational (SIA) velocities are computed at all grounded points (using Goldsby-Kohlstedt)
- ② average deformational velocity is subtracted from mass-balance velocity to give a sliding velocity
- ③ this sliding velocity is put into the MacAyeal-Morland equations at all grounded points to determine the drag coefficient which would give this much sliding

## Notes

- If deformational velocities exceed balance velocities then get negative drag! Here we set  $\beta = 10^{14} \text{ Pa s m}^{-1}$  in that case.
- Effect of high geothermal flux in Amundsen sector (from Shapiro and Ritzwoller map) is clear.

# Summary

## Our model

- ① is **multi-modal** (SIA and MacAyeal-Morland eqns for flow)
- ② is **verifiable** (and verified) for each mode of flow
- ③ solves all equations in **parallel** (PETSc)
- ④ allows choice of **grid resolution at run time**
- ⑤ includes **new earth deformation model** (*that's another talk...*)

## Planned directions

- ① consequences of different geothermal flux maps
- ② improved basal dynamics
- ③ depth-dependent density, calving criteria, ...
- ④ moving boundary between SIA and ice stream flow