

# Modeled and observed fast flow in the Greenland ice sheet

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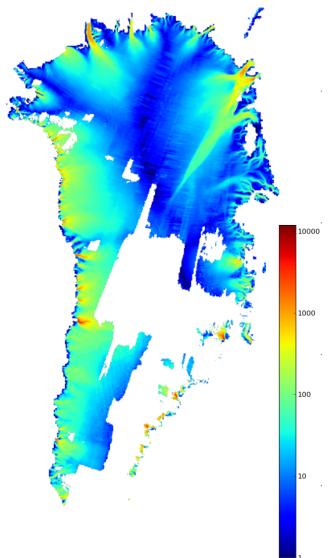
# Outline

1. Observations, and modeling goals
2. Model description
3. Results

# inSAR surface velocity observations

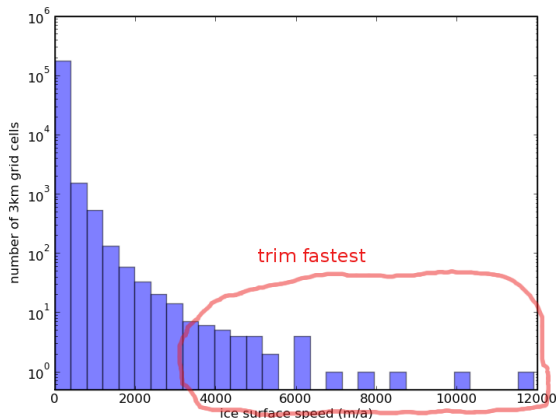
- RADARSAT SAR
- acquired Dec 2005 to Apr 2006
- inSAR and speckle-tracking to produce surface velocity<sup>a</sup> on 500 m grid
- comparison to GPS suggests errors < 10% for > 100 m/a ice; observation error much less than model error below
- here: averaged onto 3 km grid
- method: 3 km cell is kept if at least 20% of 500 m cells have values
- 71.6% area coverage on 3 km grid

<sup>a</sup>Joughin et al. [2002,2008,in preparation]



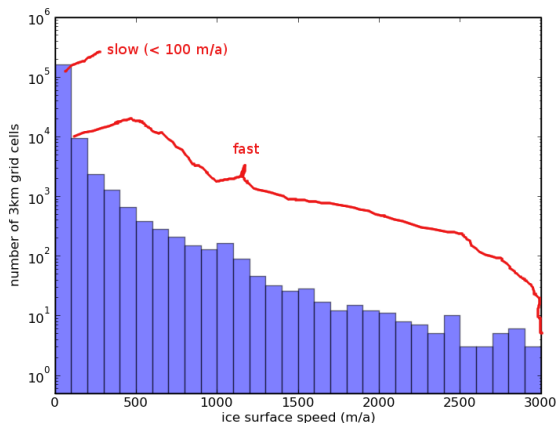
# “fast flow” versus fastest flow

- histogram of observed surface speed on 3 km grid ↓
- exist 3 km cells with  $\approx 12$  km/a surface speed
- ... but few, and in tight, steep fjord topography
- e.g. only *eleven* 3 km cells with average speed above 5000 m/a
- note log scale on  $y$ -axis
- this talk: we trim off  $> 3000$  m/a cells, for comparison to whole ice sheet model



# goal: model the fast flow

- **Definition.** *fast flow* means 100 m/a to 3000 m/a surface speed; *slow* means  $< 100$  m/a
- **Goal:** we want a model for the present dynamical state of Greenland ice sheet, with few tunable parameters, which comes close to this observed histogram →



# goal: model the fast flow 2

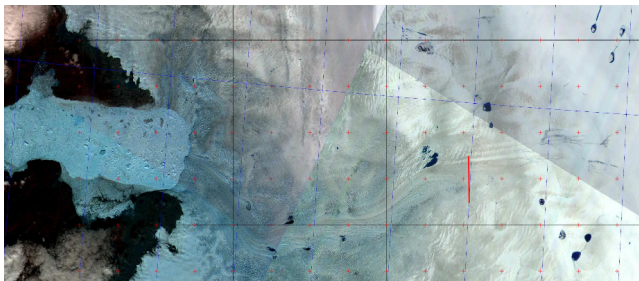
- why this particular goal?
  - \* fast-flowing regions will dominate century- and millenium-scale dynamical response to climate changes
  - \* ... especially sea level contribution
  - \* shallow models have had trouble with fast flow
  - \* a specific modeling goal focusses the mind

## goal: model fast flow 3

- is matching surface velocity enough?
  - \* no
  - \* ... but inSAR surface velocities are the highest-dimensional existing dynamical info on the present state
- why not just do inverse modeling of surface velocities?
  - \* yes, we *will* use inversion to get initial state for predictions
  - \* ... but, for prediction and scenarios, we need a model with evolving geometry, temperature, basal resistance, etc.

# the resolution challenge

- fast flow occurs
  - \* near, within, and over marginal mountain ranges
  - \* along subglacial trenches
- therefore shallow assumptions need to be removed
- *and* resolution needs to be high



5km grid (red +) and channel width (red segment) through which much of the Ilulissat (Jakobshavn) Glacier is fed

<sup>1</sup> composite ASTER image, M. Fahnestock and M. Truffer

## this talk: a small parameter study

- a small parameter study<sup>2</sup> using a hybrid shallow model
- results from eight whole Greenland ice sheet model runs
- each run: 100 model years on 3 km grid
- before start of run: spin-up in steady present climate for total of 110 k model years<sup>3</sup>
- each run starts from present bed elevation and thickness (Bamber et al 2001)
- assumed steady, present climate:
  - \* Fausto et al. (2008) temperature parameterization
  - \* PARCA accumulation map (van der Veen et al. 2001)
  - \* positive degree day scheme for surface mass balance
- at end of each run: compare surface velocities to observed

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<sup>2</sup>more below ...

<sup>3</sup>On grids refining from 10 km to 5 km to 3km. Purpose: to equilibriate ice and bedrock temperature, in balance with advection.

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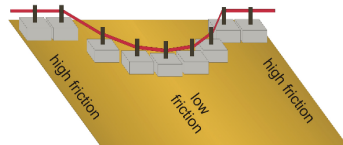
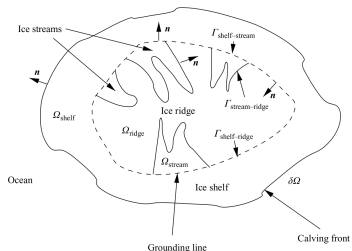
# shallow model ideas

- the Greenland ice sheet has aspect ratio  $\approx 1/1000$
- fastest-flowing parts include significant bed topography so shallow models must miss something (acknowledged!)
- “shallow” models for grounded ice include
  - \* shallow ice approximation (SIA): gravity-driven lubrication flow, sticking to bed and shearing in vertical planes; *no sliding in the SIA as understood here*
  - \* dragging shallow shelf approximation (SSA) for ice streams: gravity-driven viscous membrane sliding over variable-strength bed (“till”)

# shallow model ideas 2

## C. Schoof (2006) insight, for diagnostic case

SSA + (plastic till) = (well-posed free boundary problem for location and velocity of sliding)



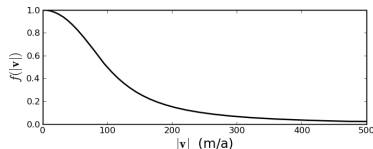
- till strength/resistance given by yield stress  $\tau_c$ :  $\vec{\tau}_b = \tau_c \mathbf{v}_b / |\mathbf{v}_b|$
- scheme is a whole ice sheet form of D. MacAyeal's individual ice stream models (1989)

# Parallel Ice Sheet Model (PISM)

- SIA and SSA velocity solutions, combined or separate
- thermomechanically-coupled
- parallel:
  - \* 3 km grid runs here done on 64, 128, or 256 processors at Arctic Region Supercomputing Center, Fairbanks
  - \*  $501 \times 935 \times 201$  ice grid;  $\approx 300$  million temperature and velocity unknowns
  - \* all runs here total  $\approx 8000$  processor-hours
  - \* is that a lot of processor-hours?
- homepage      [www.pism-docs.org](http://www.pism-docs.org)

# PISM: Schoof ideas adapted to prognostic modeling

- SSA-as-a-sliding law (Bueler et al. 2009)
  - \*  $\mathbf{U} = f(|\mathbf{v}|)\mathbf{u} + (1 - f(|\mathbf{v}|)) \mathbf{v}$ , where
  - \*  $\mathbf{v}$  is SSA solution
  - \*  $\mathbf{u}$  is SIA solution
  - \*  $\mathbf{U}$  is model velocity used in mass continuity and energy conservation equations



- pseudo-plasticity:

$$\vec{\tau}_b = \tau_c \frac{\mathbf{v}_b}{|\mathbf{v}_b|^{1-q} (100 \text{ m/a})^q}$$

- surround ice sheet by thin notional ice shelf to maintain ellipticity of SSA

# PISM: (*newly!*) polythermal by enthalpy method

- Aschwanden and Blatter (2008 JGR; in preparation 2009)
- $E$ =enthalpy=(sensible thermal + latent thermal + potential of pressure)
- temperature  $T$  and liquid water fraction  $\omega$  are functions of enthalpy and pressure, for cold and temperate ice:

$$T = T(E, p), \quad \omega = \omega(E, p)$$

- *think*:  $E = E(t, x, y, z)$  is the primal thermal variable in conservation of energy equation
- solve conservation of energy equation for  $E$

# PISM: basal thermo-mechanical model

- yield stress determined by Mohr-Coulomb:

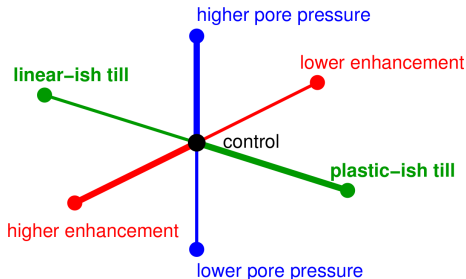
$$\tau_c = c_0 + (\tan \phi) (\rho g H - p_w)$$

- $c_0 = 0$
- basal melt rate from 1 %  $\omega$  rule (Greve 1997)
- pore water pressure  $p_w$  is local, time-integrated function of basal melt rate
- till friction angle  $\phi$  determined by bed elevation below sea level
  - \* motivated by presumed marine history of sediment below sea level (Huybrechts and de Wolde 1999)
  - \*  $\phi = 5^\circ$  at -700 m and below
  - \*  $\phi = 20^\circ$  at +300 m and above
  - \* linear between
- model description done!

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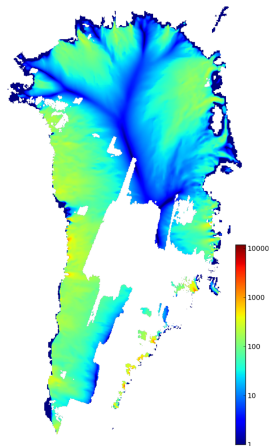
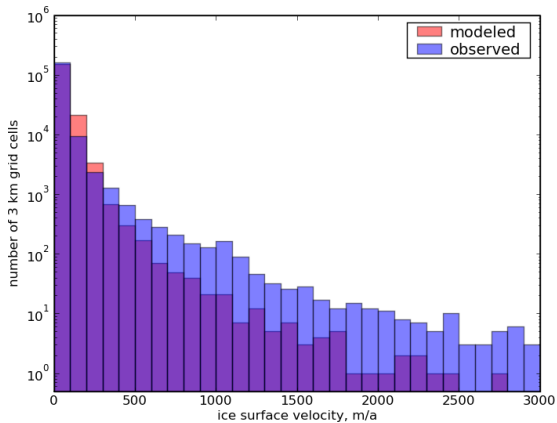
# parameter study: control run plus six variations



- enhancement factor  $e$ : 1, 3, 5
- exponent  $q$  in basal power law; 0=plastic, 1=linear: 0.50, 0.25, 0.10
- limit  $p_{\max}$  on pore water pressure; % of overburden: 95, 98, 99
- first directly affects only SIA velocities, last two directly affect only SSA velocities

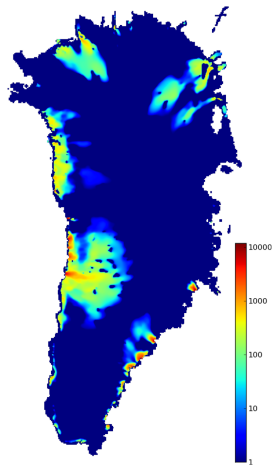
# Control run results

- enhancement factor=3, limit on pore water pressure=98%, exponent in basal power law=0.25



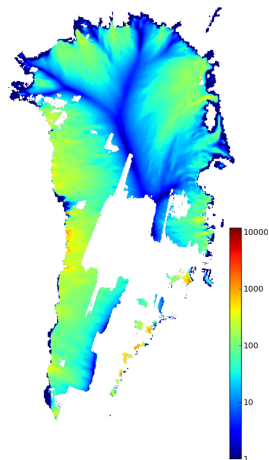
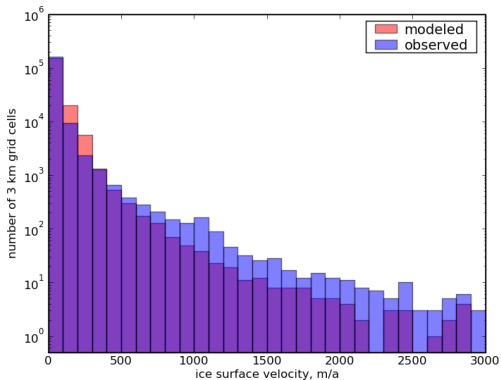
## Control run results 2: how much is from sliding?

- sliding speed, on same velocity scale



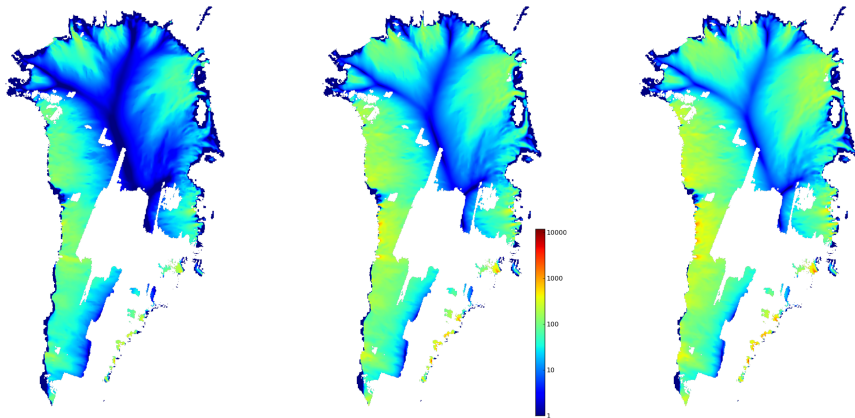
# Control run results 3: what if there is no sliding at all?

- enhancement factor=3 and no SSA computation (no sliding; SIA only; “sub-control” run?)
- SIA-only models with no sliding give reasonable distribution of fast flow, if done on 3 km grid
- distinction from with-SSA-sliding runs seen in time-dependence ... another talk ...



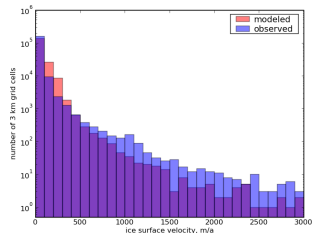
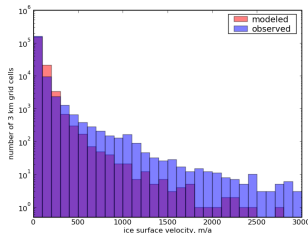
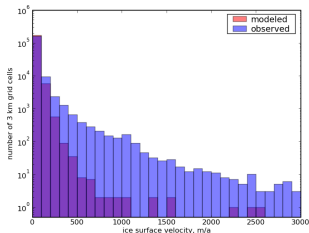
# Enhancement factor axis

lower enhancement      control      higher enhancement



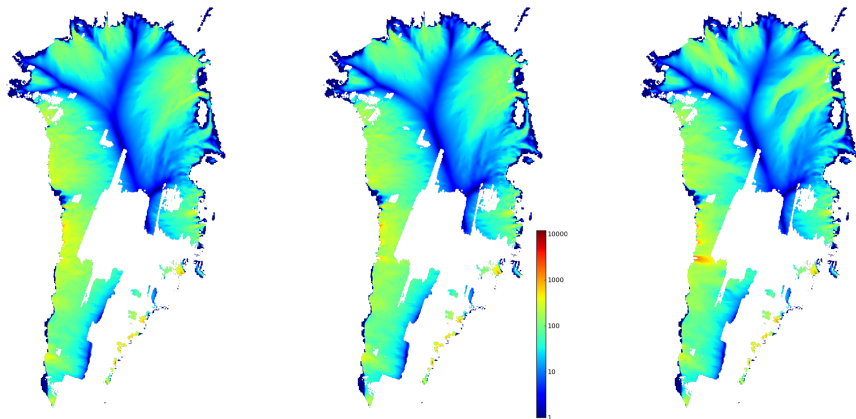
# Enhancement factor axis 2

lower enhancement      control      higher enhancement

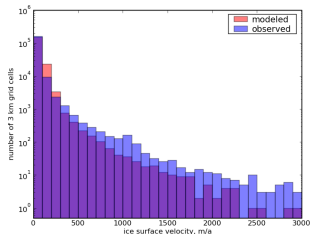
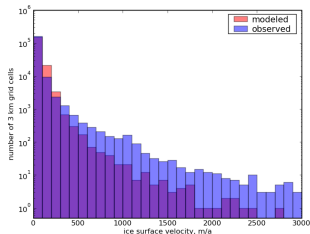
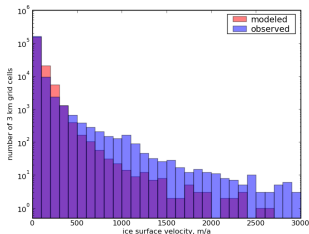
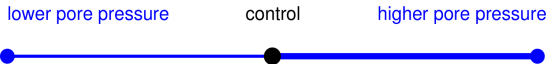


# Allowed pore water pressure axis

lower pore pressure      control      higher pore pressure



# Allowed pore water pressure axis 2

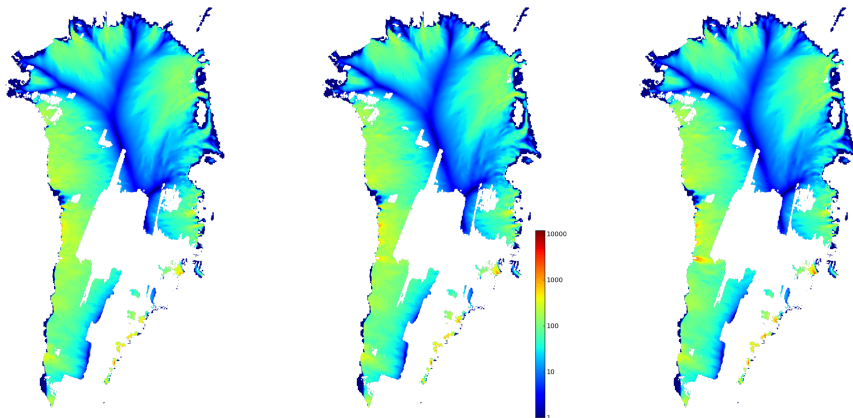


# Plasticity (power law power) axis

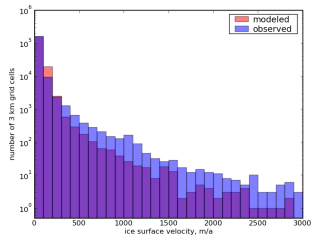
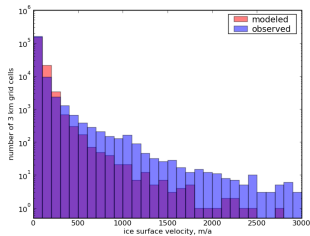
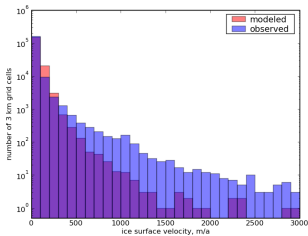
linear-ish till

control

plastic-ish till



# Plasticity (power law power) axis 2



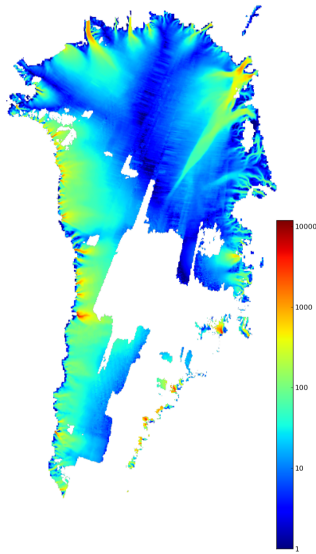
# Summary of results

- high resolution is a key to modeling fast flow, regardless of shallowness
- SIA models can yield fast flow, but then too much is in the 100 m/a to 300 m/a range, compared to observed
- evidence here for two parameters effecting fast flow in Greenland:
  - \* high subglacial water pressure
  - \* plastic or nearly-plastic till behavior

# Conclusions

- the SSA is a shallow sliding law
  - \* which balances basal shear by membrane stresses
  - \* ... but it requires a parameterization of subglacial “wet and soft” processes
- enthalpy-formulated polythermal ice models are
  - \* easy to implement, and
  - \* add credibility to conservation of energy and drainage models
- parallelism is effective
- 3 km grid or finer Greenland ice sheet models with ice streams *will contribute to IPCC AR5*
- next steps:
  - \* inverse modeling for initialization
  - \* better basal and surface process modeling
  - \* more complete stress balances for outlet glaciers
- The End

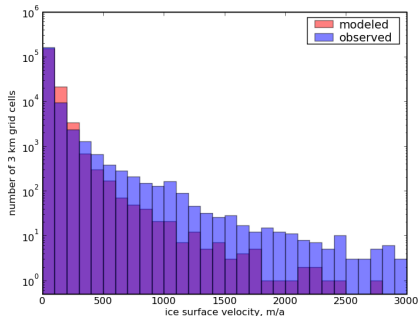
# inSAR surface velocity for Greenland



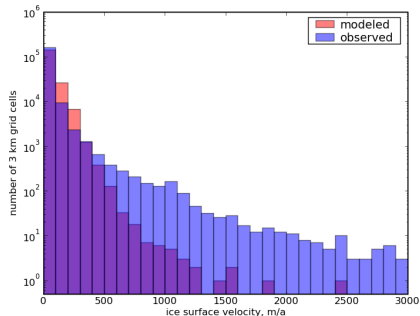
## Extra: Control run results 4: what happened at 20 model years?

- previous results were at 100 model years; here is an example at 20 model years

control run at 100 a



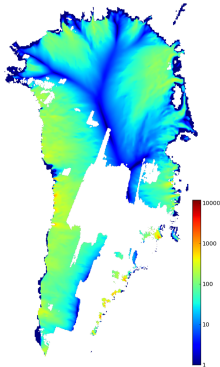
control run at 20 a



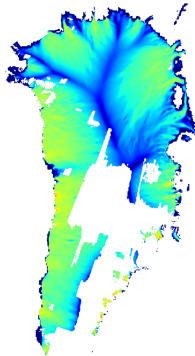
# Extra: Geothermal high at source of NE Greenland

- following Fahnstock et al (2001), try a 970 mW m<sup>-2</sup> “hot spot”

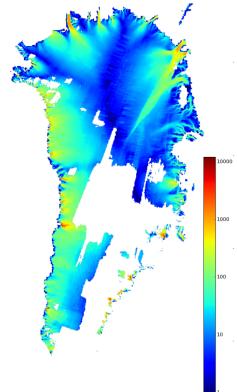
control



hotspot



observed



# PISM, cont.

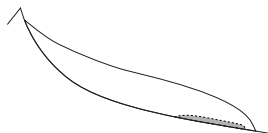
- verifiability
  - construction of verification tests main focus during development (Bueler et al. 2005,2007)
  - tests for SIA, SSA, and thermo- components
  - can be checked at any time
- derivability
  - its a big C++ program
  - Potsdam group (Levermann et al.) has PISM-PIK Antarctic model with improved ice shelf dynamics and fracture-based calving

# PISM: polythermal by enthalpy method 2

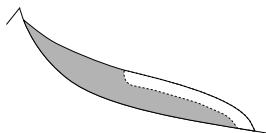
- conductivity of polythermal ice:

$$k = \begin{cases} k_{\text{ice}}, & T(E, p) < T_{\text{pmp}} \\ 0, & T(E, p) = T_{\text{pmp}} \end{cases}$$

- flow law is Paterson & Budd (1982) with Lliboutry & Duval (1985) dependence on  $\omega$
- cold-temperate transition surface (CTS) is boundary of  $\omega > 0$  region
- ... so we have no explicit representation of CTS as a surface
- ... and no restriction on evolving CTS shape



Canadian-type



Scandinavian-type